7R5\_ 249\_250 Reg. Nos. 768-769. Luck Brothers, Dulverton

# COMPARISON OF EXTRUSION AND PRESSING OF BRICKS FROM CLAY AND SHALE

by F. C. Gillespie.

## SUMMARY

Samples of clay and shale obtained by Mr. F. C. Gillespie on the 28th July, 1960, from the Dulverton quarry of Luck Bros. Pty. Ltd., have been tested for suitability for brick production by extrusion, in comparison with the stiff-plastic pressing method. The red and black materials were tested separately, and also in a blend with proportions two to one respectively.

Little difference was found in the working properties of the red and black materials, but the latter had a considerably shorter firing range, and this characteristic was also evident in the blend. Extrusion without de-airing was unsatisfactory, but de-aired extruded briquettes were superior in strength and appearance to the pressed specimens, and were adequately fired for facing bricks at 900°C. For full sized extruded brick production, perforation would be desirable to facilitate drying and firing.

#### DESCRIPTION

Reg. No. 768. Sample of red and white clay and shale, taken from the top portion of the quarry face.

Reg. No. 769. Sample of black shale, taken from the bottom portion of the quarry face.

Blend No. B19. Two parts of No. 768 and one part of No. 769.

# PREPARATION AND TESTING

Each material was crushed wet, by passing three times through high speed rolls, with the gap set initially to approximately three-eighths of an inch, then reduced to one-quarter of an inch, and finally one-eighth of an inch. Water was added as required, and mixing carried out in a pug mill, which simultaneously formed the clots for stiff-plastic pressing.

Briquettes produced either by pressing in a screw press, or by extrusion in an auger machine, were dried, (test specimens were placed in an oven at 50°C and the temperature slowly raised to reach 110°C in 1½ hours), and fired at various temperatures, soaking for two hours. Fired briquettes were tested for efflorescence.

#### RESULTS

## I-Forming

| Material | Forming<br>Method      | Tempering<br>Moisture (%   | Remarks   |
|----------|------------------------|--|---|
| 768 {    | S.P.<br>N.D.A.<br>D.A. | $\begin{array}{c} 21\frac{1}{2} \\ 23\frac{1}{2} \\ 23\frac{1}{2} \end{array}$ | Laminates readily; warps slightly.<br>Dog-ears badly; laminates.<br>Clean, firm and very strong.            |
| 769 {    | S.P.<br>N.D.A.         | 19½<br>21½   | Laminates readily; requires considerable oil lubrication; warps slightly.  Dog-ears badly; laminates; weak. |
|          | D.A.                   | $\tilde{2}^{12}_{1}$   | Very clean, firm and strong.  |
| B19      | S.P.                   | 21   | Laminates readily; requires considerable oil lubrication; warps slightly.                                   |
| 1        | N.D.A.<br>D.A.         | $\frac{22\frac{1}{2}}{22\frac{1}{2}}$  | Dog-ears and laminates badly.<br>Very clean, firm and strong.   |
|          | Note-                  | N.D.A. = 1   | stiff-plastic pressed.<br>Not de-aired extruded.<br>De-aired extruded.                                      |

## II-Drying and Firing

| Material | Forming<br>Method | $\begin{array}{c} Drying \\ Contraction \\ \begin{array}{c} 0 \\ 5\frac{1}{2} \\ 7\frac{1}{2} \\ 8 \end{array}$ | Total Contraction after Firing (%) |       |                            |                |               |         |
|----------|-------------------|---|------------------------------------|-------|----------------------------|----------------|---------------|---------|
| (        | S.P.              |   | 850°C<br>6                         | 900°C | 950°C<br>8½                | 1,000°C<br>12½ | 1,050°C<br>15 | 1,100°C |
| 768      | N.D.A.<br>D.A.    |   |                                    | iò    | 11                         | 151            | 161           | 161     |
| 769 {    | 8.P.<br>N.D.A.    | 4 ½<br>5 ½  |                                    | 7     | 91                         | 11(S.B         | (B)           | -       |
|          | D.A.              | 6   | $6\frac{1}{2}$                     | 9     | $\frac{10}{10\frac{1}{2}}$ | 121            | (B)           | **      |
| В19 {    | S.P.              | 5   | 6                                  | 61    | 9                          | 12             | (B)           | 616.50  |
|          | N.D.A.<br>D.A.    | 6<br>6½   | 7                                  | 81    | 10<br>11                   | 14(S.B         | (B)           | 1000    |
|          | Note-             |   | atly bloat                         | ed.   |                            |                |               |         |

Bloated and partially fused.

All briquettes withstood the oven drying test except Nos. 769 N.D.A. and B19 S.P., both of which cracked badly.

All stiff-plastic briquettes developed moderate cracks during firing, No. 769 being least affected in this way. De-aired briquettes fired at 850°C cracked during cooling, but no cracks occurred in de-aired specimens fired at 900°C or higher.

The approximate firing ranges of these materials are given in the following table:-Firing Pance (°C)

| Material | Stiff-plastic Pressed | De-aired Extruded |
|----------|-----------------------|-------------------|
| 768      | 950 — 1050            | 900 - 1050        |
| 769      | 950                   | 900 — 1000        |
| B19      | 950 — 1000            | 900 — 950         |
|          |                       |                   |

## II—Efflorescence

Two types of efflorescence occurred on the briquettes tested; a yellow material identified as a vanadium compound, and white crystals consisting mainly of magnesium sulphate. The vanadium efflorescence appeared on almost all briquettes fired below 1000°C, but was not detected on those fired above that temperature. The magnesium sulphate was very irregularly distributed, but mainly confined to No. 769; it did not appear on briquettes fired above 1000°C.