

## **10.9 FORMATION INTEGRITY TESTS**

The hesitation method shall be used for the conduct of all Formation Integrity Tests. This involves pumping a small amount, waiting for the pressure to stabilise before repeating the process until the maximum test pressure is achieved. The test pressure shall be limited to a maximum pressure that does not exceed the lowest of the following:

- Actual leak-off pressure.
- The pressure specified in the Drilling Programme (typically the pressure required to give required kick tolerance or 80% of casing burst pressure).
- The wellhead test pressure.
- The BOP test pressure.
- A maximum pressure of 0.8 psi/ft at the casing shoe.

### **10.9.1 Responsibilities**

All responsibilities for Formation Integrity Testing are given in Section 10.2

### **10.9.2 Testing Preparation**

The following equipment is recommended for execution of a Formation Integrity Test, for accuracy and control:

- Pumping unit with tanks calibrated in ¼ barrel increments.
- Calibrated gauges covering anticipated pressure ranges mounted on a manifold.
- Chart recorder.

### **10.9.3 Test Procedure**

The following procedure shall be adhered to when performing a Formation Integrity Test:

1. Drill out cement plus 3 m of new formation.
2. Circulate clean to a balanced mud weight (use old mud from previous section).
3. Pull the bit back in casing shoe.
4. Make sure the hole is filled up and close the annular BOP (Hydriil) around the drill pipe.
5. Rig up the pump to the drill pipe. Use a pressure gauge of appropriate range (0 - 1,500 psi.), mounted at the pump unit manifold.
6. Slowly pump mud until pressures begin to increase. Volume pumped will start from this point.
7. Pump 0.125 - 0.25 bbl and wait for 2 minutes or the time required for the pressure to stabilise in the case this takes longer.
8. Record the volume pumped, and the bleed back stabilised pressure.
9. Repeat items 6 & 7 and plot pressures versus cumulative mud volume
10. Continue procedure until either the final stabilised pressure, after the waiting time, deviates from the expected pressure from the plot or the required maximum pressure is reached.
11. Keep well closed in to verify that a constant pressure has indeed been obtained.
12. Release pressure and record volume recovered in tank.

#### 10.9.4 Calculations

Formation Intake Gradient (FIG)

$$\text{FIG} = \frac{\text{LOP} + (\text{CSD} \times \text{MG})}{(\text{CSD} - \text{RKBE})} \text{ psi/ft}$$

Effective Mud Gradient (EMG)

$$\text{EMG} = \frac{\text{LOP} + (\text{CSD} \times \text{MG})}{\text{CSD}} \text{ psi/ft}$$

Maximum Allowable Annular Surface Pressure (MAASP)

$$\text{MAASP} = \text{LOP} - (\text{CSD} \times \text{MG}) \text{ psi}$$

Formation Breakdown Pressure (FBP)

$$\text{FBP} = \text{LOP} + (\text{CSD} \times \text{MG})$$

Where:

|      |   |   |
|------|---|---|
| LOP  | = | Leak-Off Pressure (psi),<br>surface pressure recorded during the test |
| CSD  | = | Shoe Depth of last casing set (TVD ft RKB)                            |
| MG   | = | Mud Gradient (psi/ft)   |
| RKBE | = | Rotary Kelly bushing elevation above ground level (ft)                |

## APPENDIX 1: GENERAL WELL CONTROL FORMULAE

### 1. The Formation Pressure ( $P_0$ )

$$P_0 = P_{dp} + (D_h \times \rho_1) \text{ psi}$$

$P_0$  = Formation Pressure (psi)

$P_{dp}$  = Shut in drill pipe pressure (psi)

$D_h$  = Depth of hole (ft)

$\rho_1$  = Formation pressure gradient (psi/ft)

### 2. The new mud gradient to balance $P_0$ ( $\rho_2$ )

$$\rho_2 = P_0 \div D_h \text{ psi/ft}$$

### 3. The height of the influx ( $h_{inf}$ )

$$h_{inf} = V_{inf} \div CAP_{ann} \text{ ft}$$

$V_{inf}$  = Volume of influx (bbl)

$CAP_{ann}$  = Annular capacity (bbl/ft)

### 4. The gradient of the influx ( $\rho_{inf}$ )

$$\rho_{inf} = \rho_1 - (P_{ann} - P_{dp}) \div h_{inf} \text{ psi/ft}$$

$P_{ann}$  = Shut in casing pressure (psi)

### 5. Type of influx

$\rho_{inf} < 0.2$  psi/ft is gas

$\rho_{inf} < 0.35 - 0.39$  psi/ft is crude oil

$\rho_{inf} < 0.433$  psi/ft is water

$\rho_{inf} < 0.433 - 0.465$  psi/ft is salt water

### 6. Volumes

#### Contents of string

$$V_{str} = CAP_{dp} \times (D_h - L_{dc}) + CAP_{dc} \times L_{dc} \text{ bbls}$$

$V_{str}$  = Volume of string (bbl)

$CAP_{dp}$  = Capacity of dp (bbl/ft)

$L_{dc}$  = Length drill collars (ft)

$CAP_{dc}$  = Capacity of dc (bbl/ft)

$L_{dc-oh}$  = Length dc in oh (ft)

#### Contents of annulus open hole section

$$V_{dc-oh} = CAP_{dc-oh} \times L_{dc-oh} \text{ bbls}$$

$V_{dc-oh}$  = volume between oh and dc (bbl)

$CAP_{dc-oh}$  = Capacity between dc and oh (bbl/ft)

$V_{dp-oh}$  = volume between oh and dp (bbl)

$CAP_{dp-oh}$  = Capacity between dp and oh (bbl/ft)

$L_{dp-oh}$  = Length dp in oh (ft)

$V_{csg-dp}$  = volume between csg and dp (bbl)

$CAP_{csg-oh}$  = Capacity between csg and oh (bbl/ft)

$D_{csg}$  = Depth of casing (ft)

$$V_{dp-oh} = CAP_{dp-oh} \times L_{dp-oh} \text{ bbls}$$

#### Contents of annulus casing section

$$V_{csg-dp} = CAP_{csg-dp} \times D_{csg} \text{ bbls}$$

### 7. Pre kick calculations

$$1. \text{ MAASP} = (\rho_{fs} - \rho_1) \times D_{csg} \text{ psi}$$

$$2. \text{ CAP}_{str} = 9.7138 \times \phi_{id \text{ pipe}}^2 \times 10^{-4} \text{ bbls/ft}$$

**Note:** 1)  $\phi_{id \text{ pipe}}$  in inches. 2)  $\text{CAP}_{str} = \text{CAP}_{dp} + \text{CAP}_{dc} + \text{etc.}$

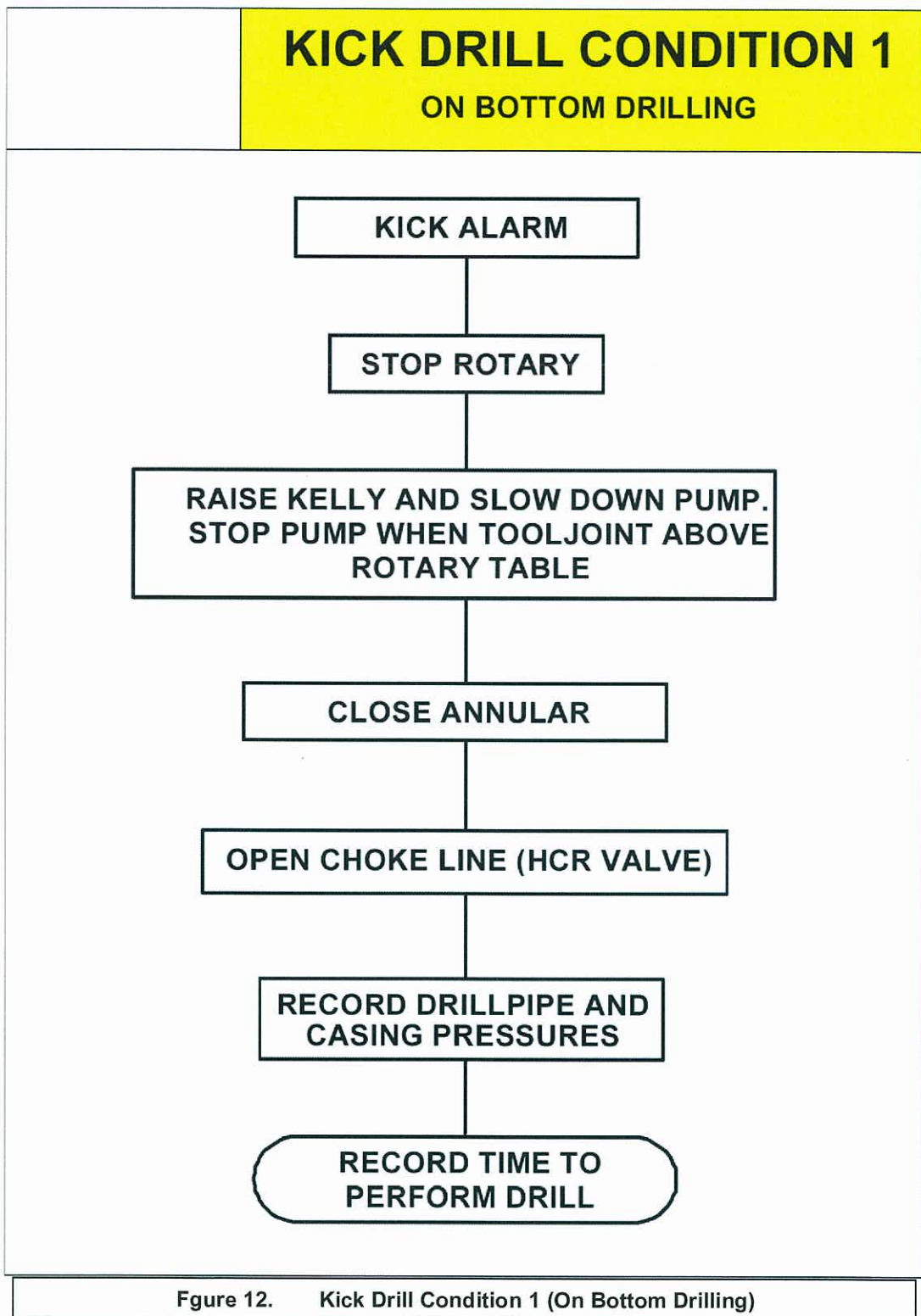
$$3. \text{ CAP}_{ann} = 9.7138 \times (\phi_{id \text{ hole}}^2 - \phi_{id \text{ pipe}}^2) \times 10^{-4} \text{ bbls/ft}$$

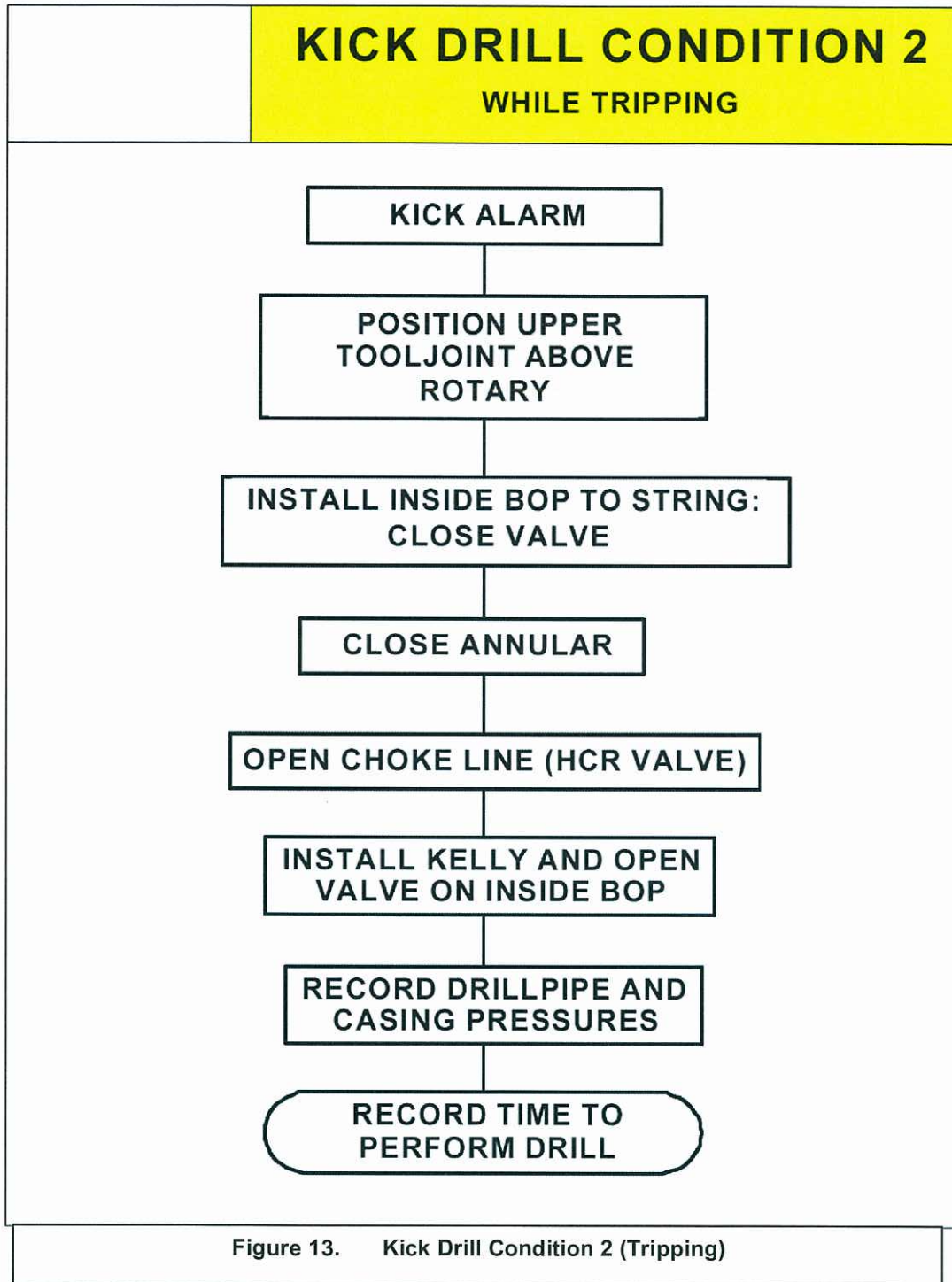
**Note:** 1)  $\phi$  in inches 2)  $\text{CAP}_{ann} = \text{CAP}_{dc-oh} + \text{CAP}_{dp-oh} + \text{CAP}_{dp-csg} + \text{etc.}$

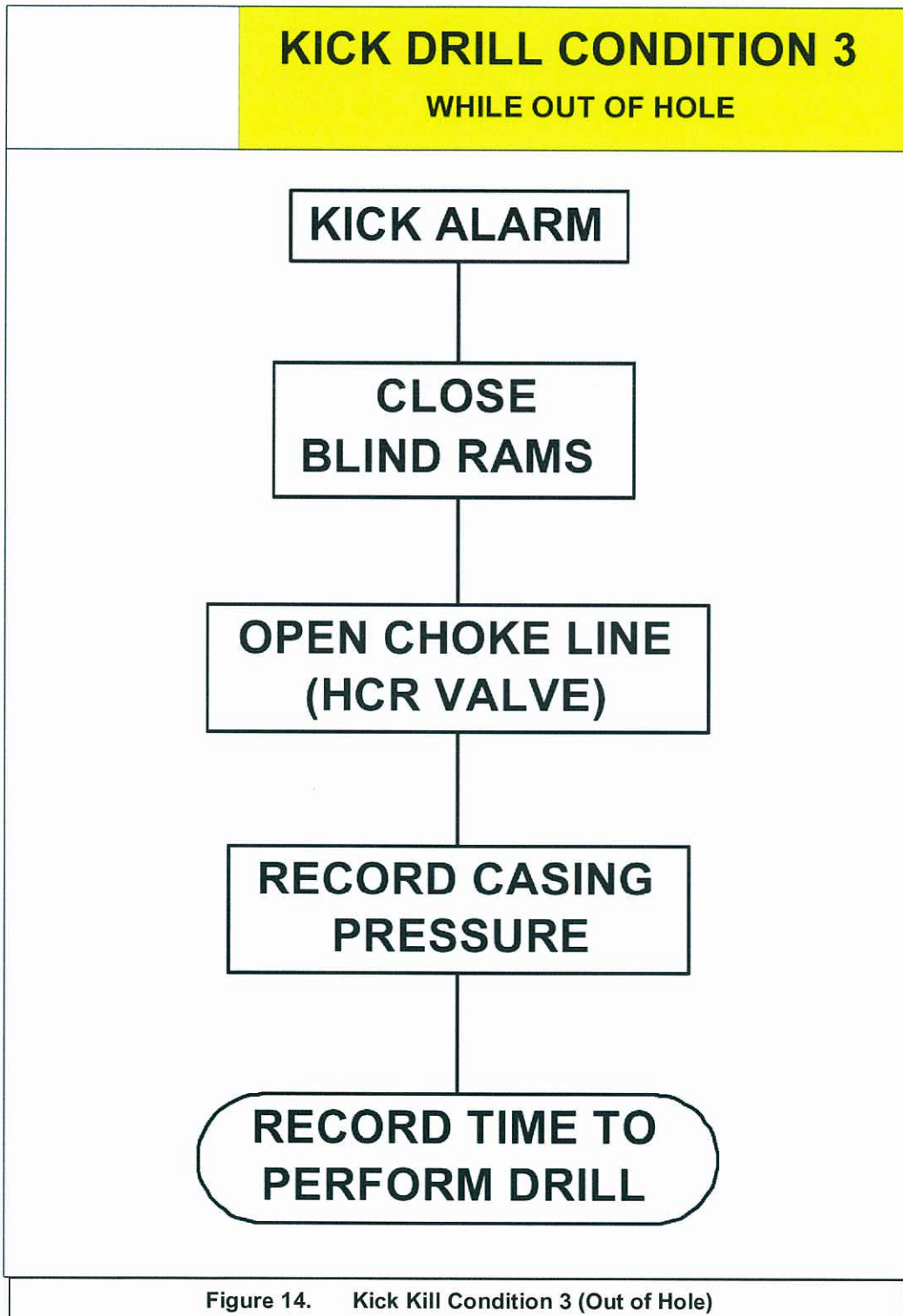
## Appendix II: Well Control Schematic Procedures

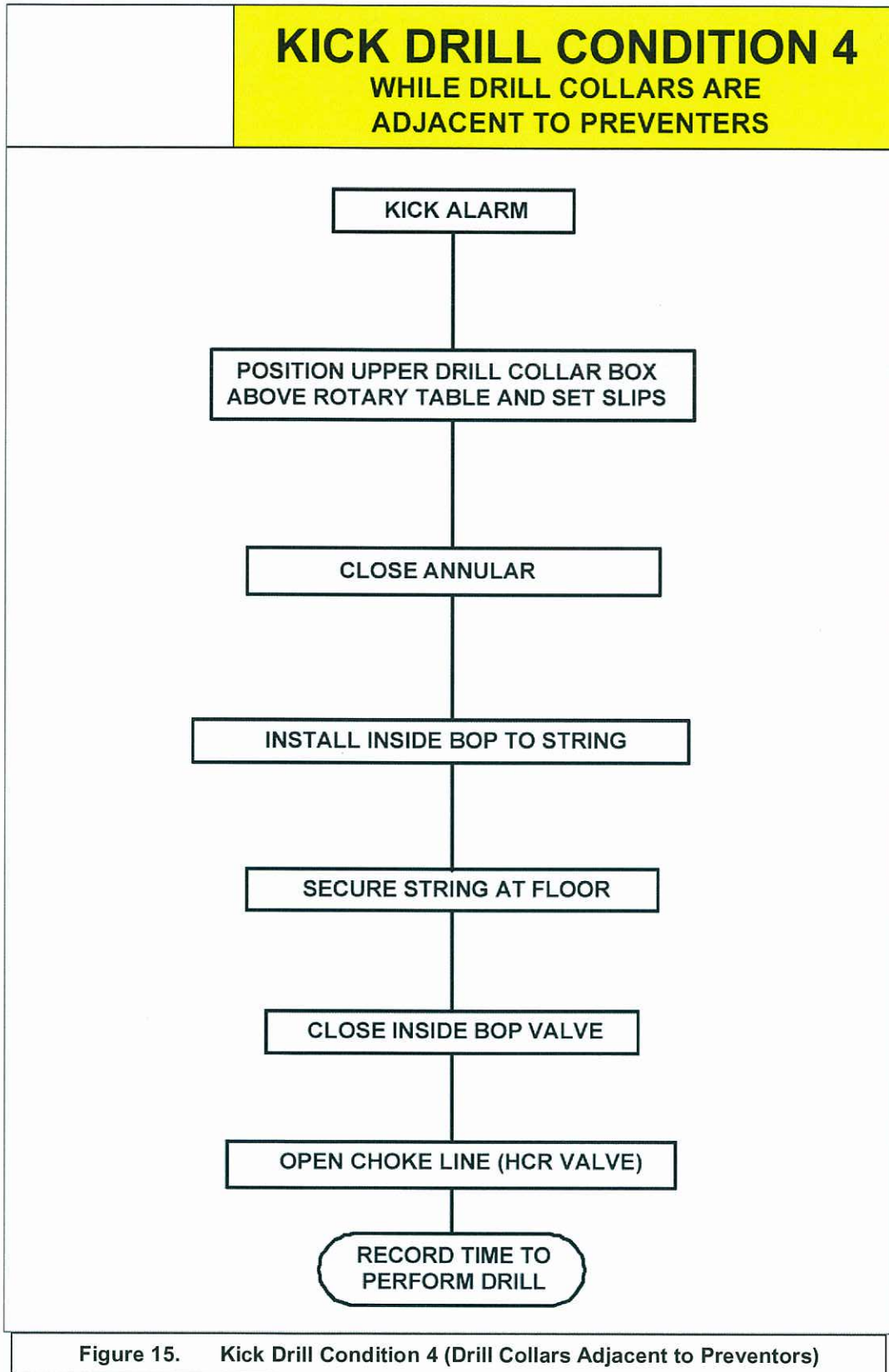
This Chapter contains the following schematic representations of the key well control procedures described in this Manual:

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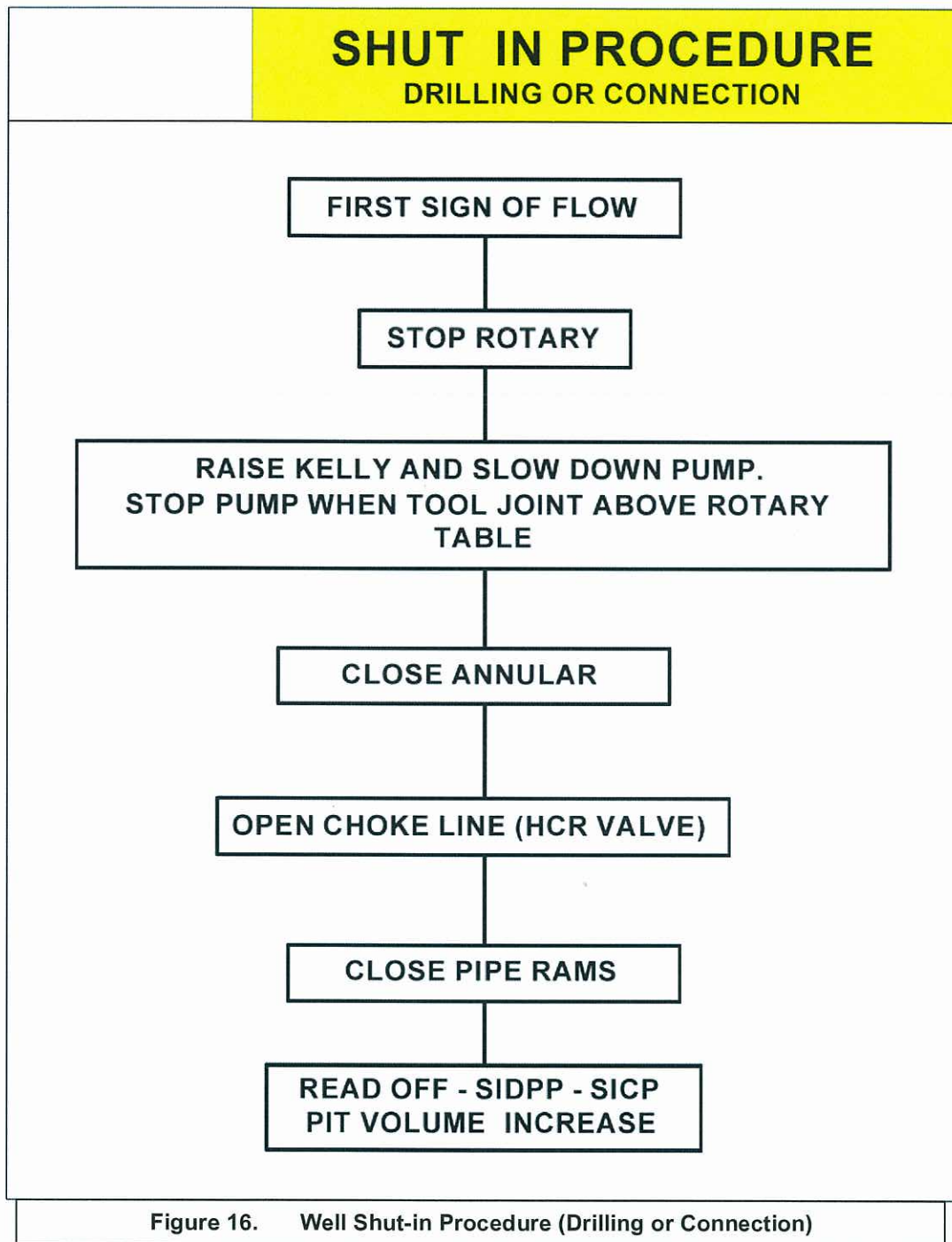


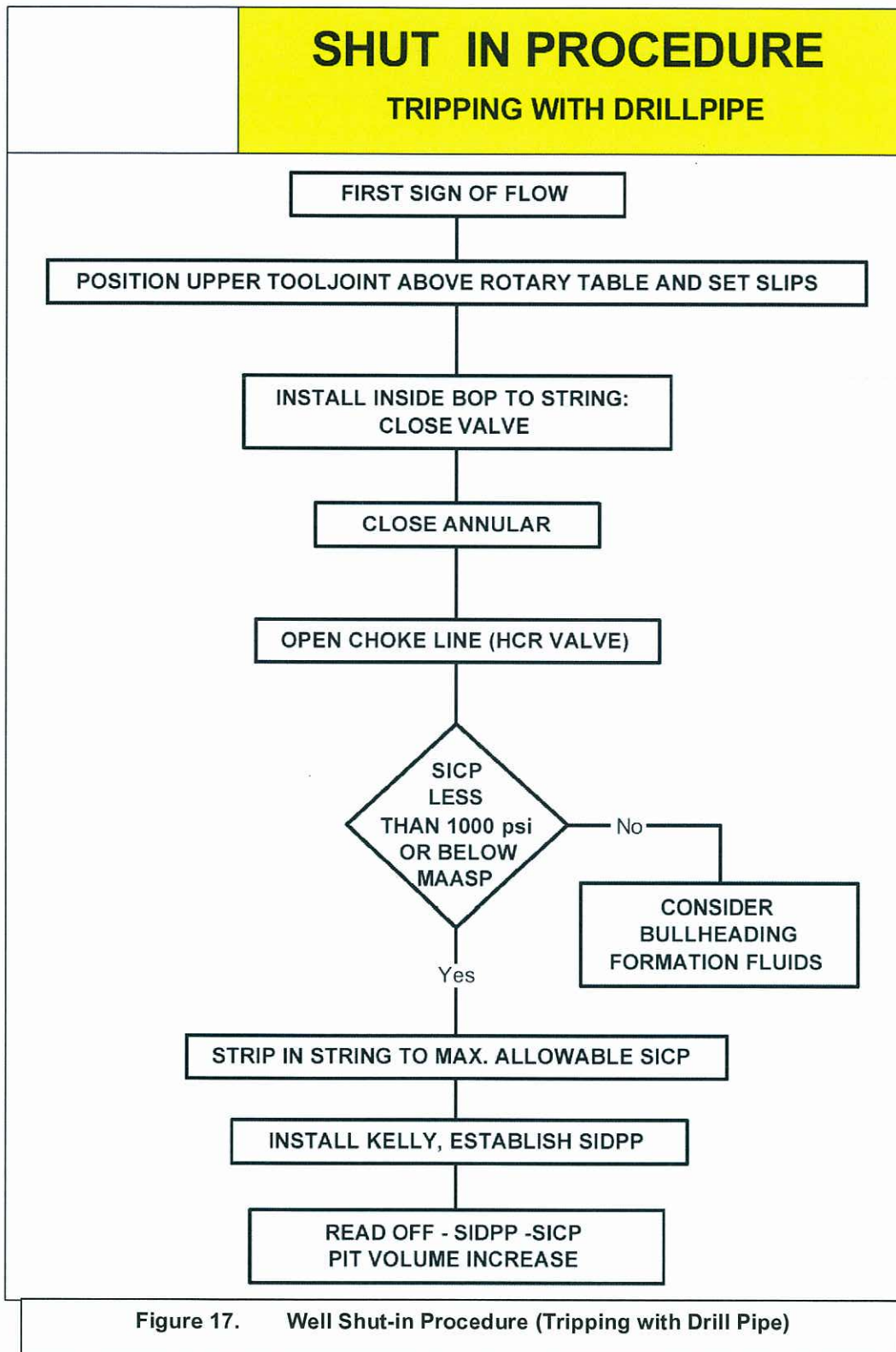


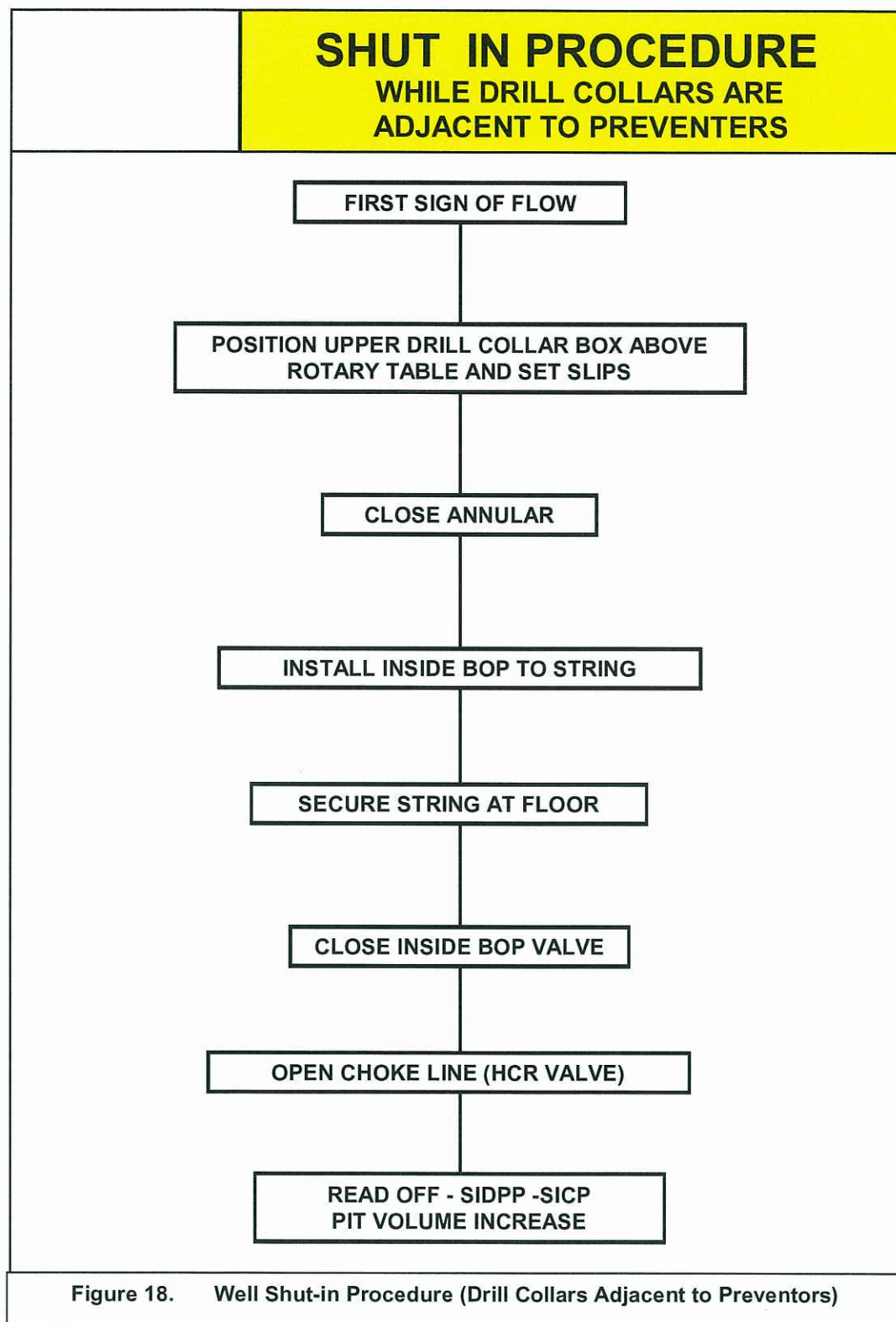












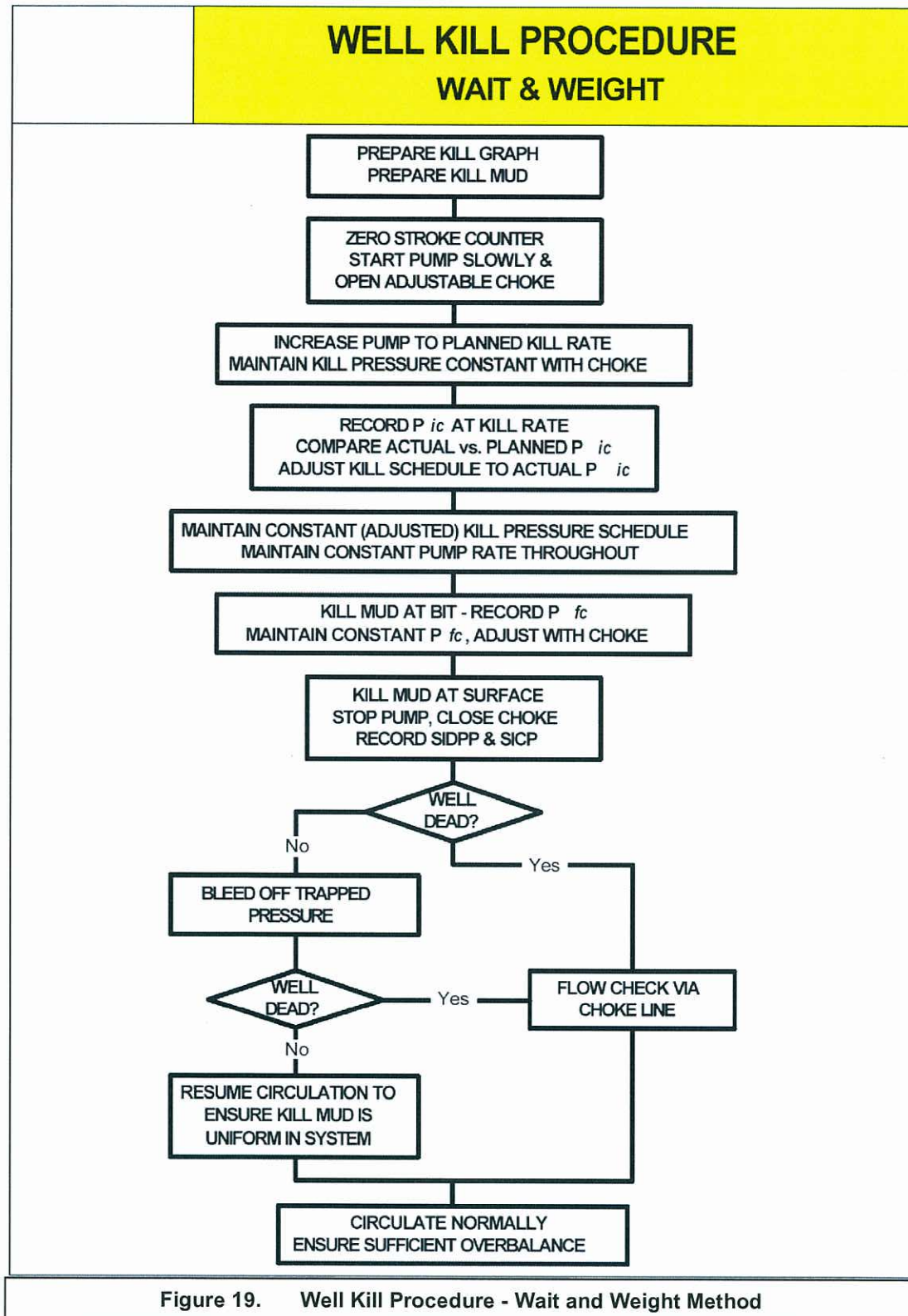
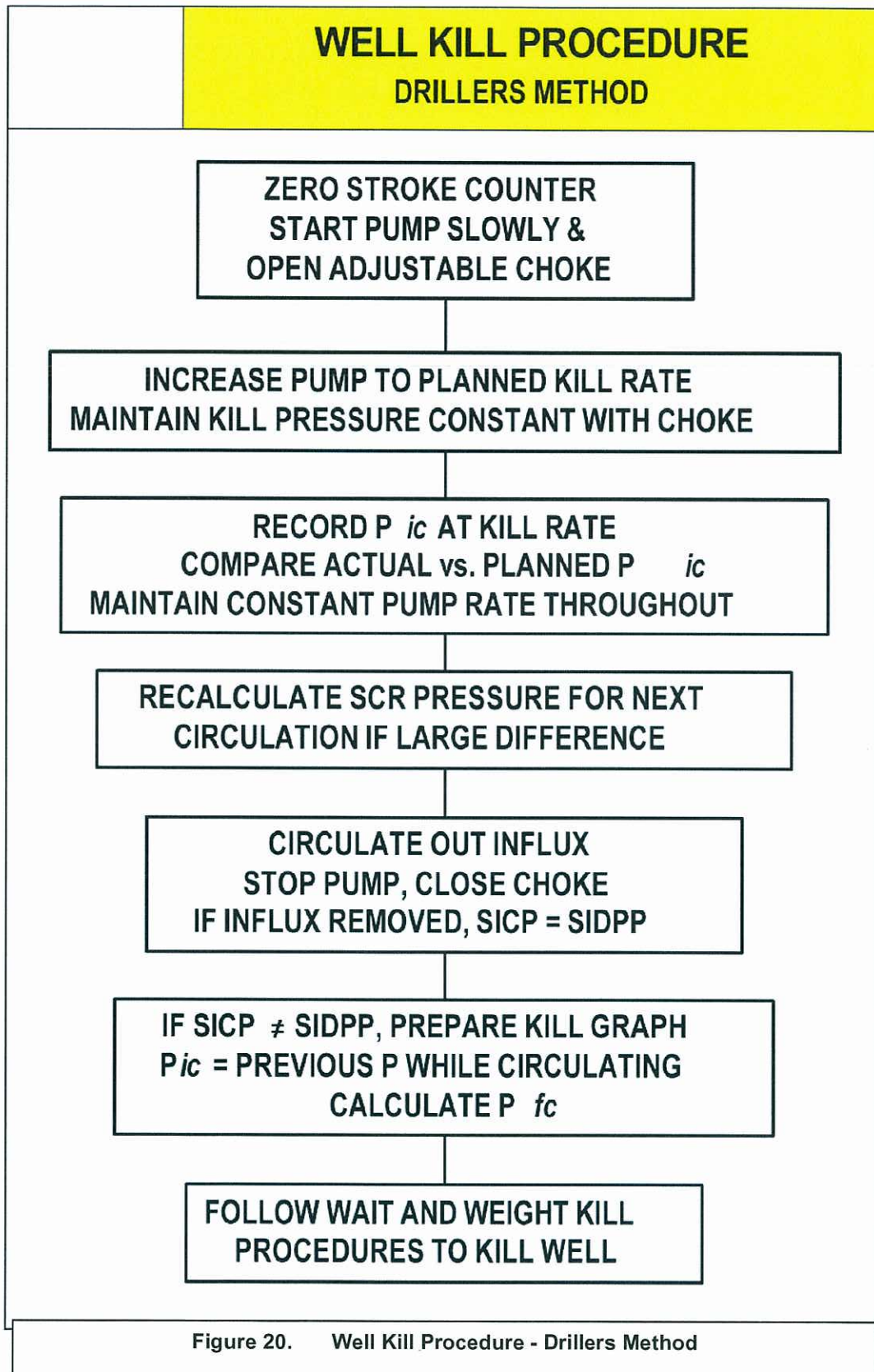
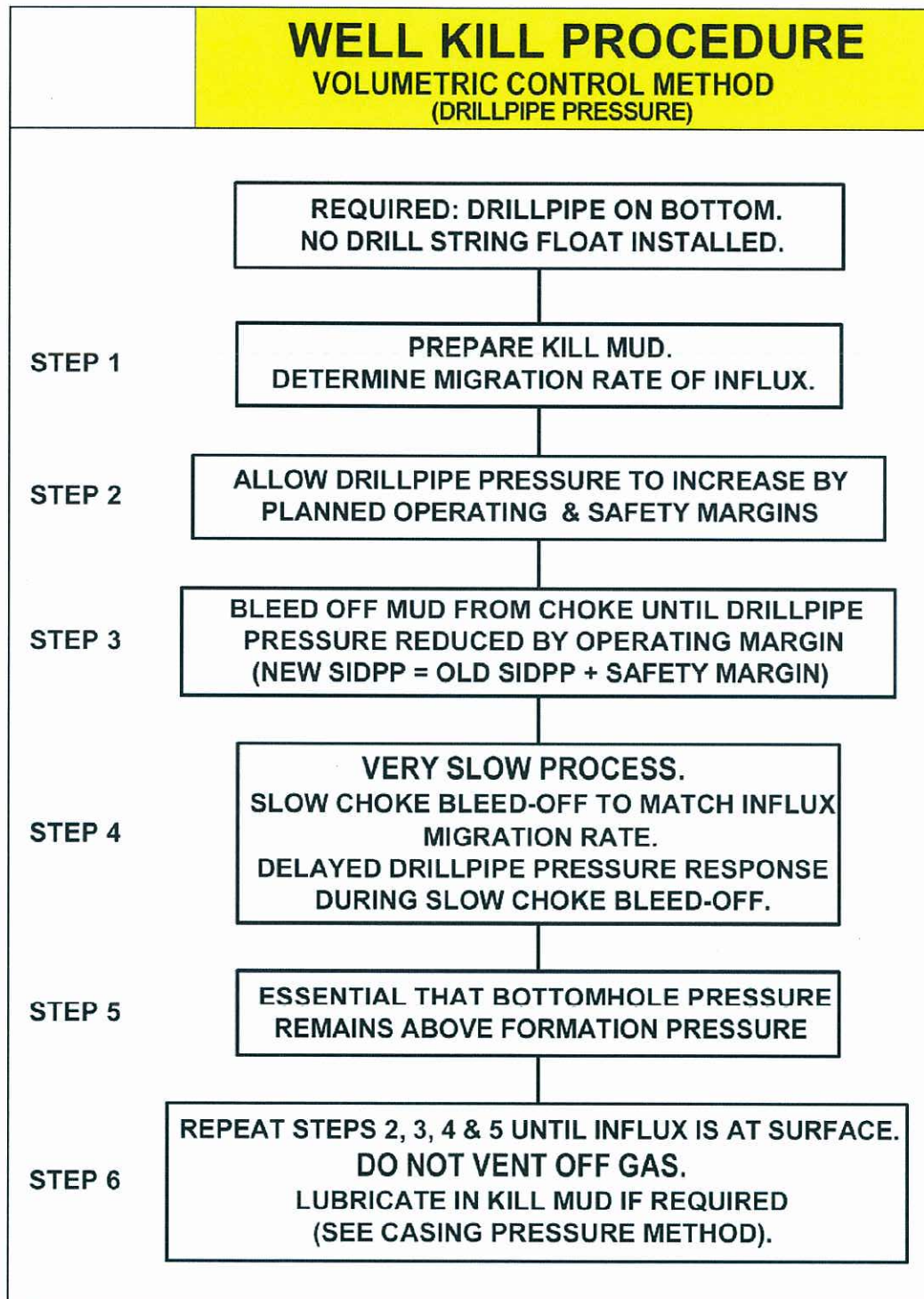


Figure 19. Well Kill Procedure - Wait and Weight Method







*Well Control Procedure - Volumetric Control Method (Drill pipe pressure)*

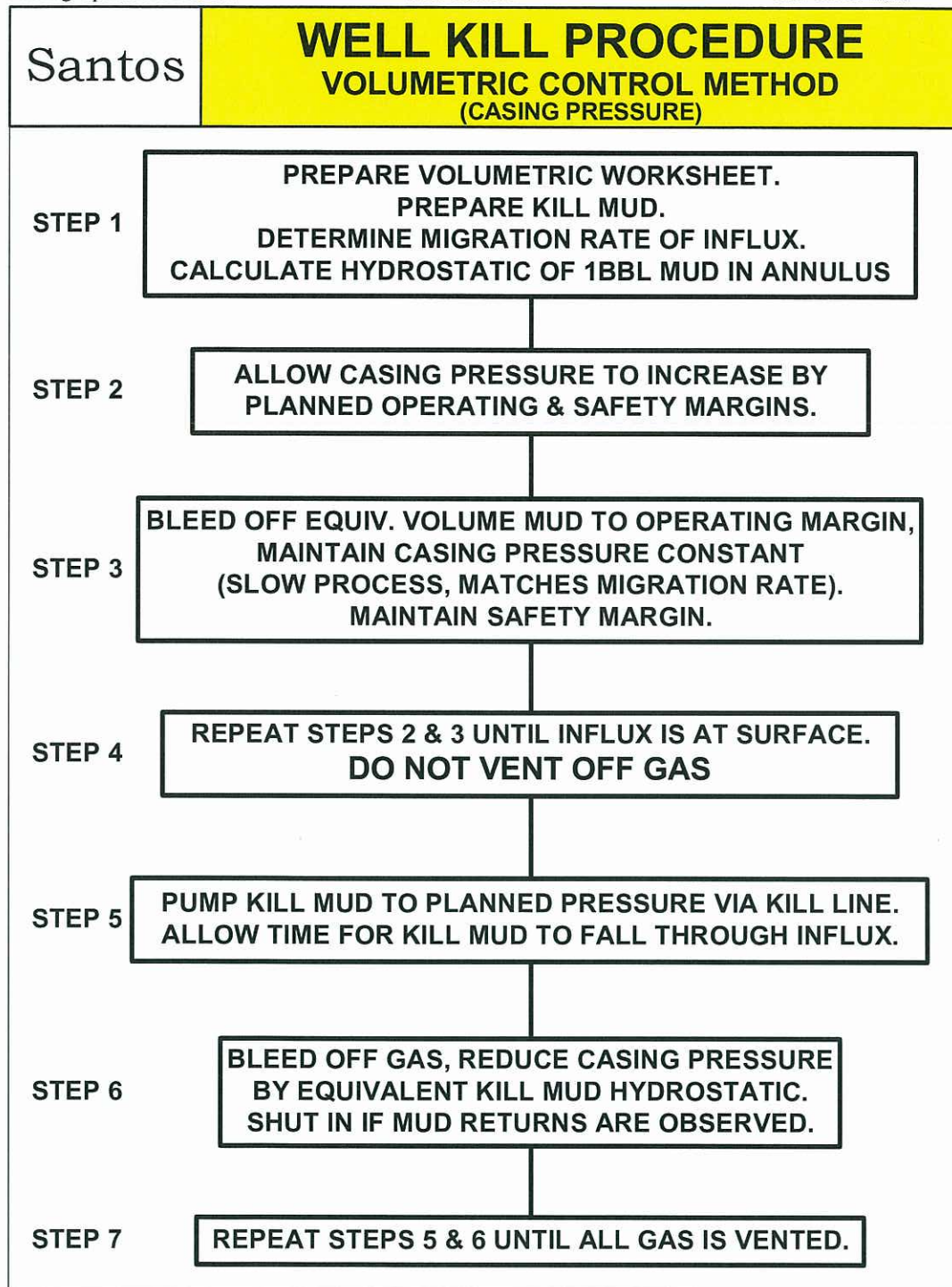
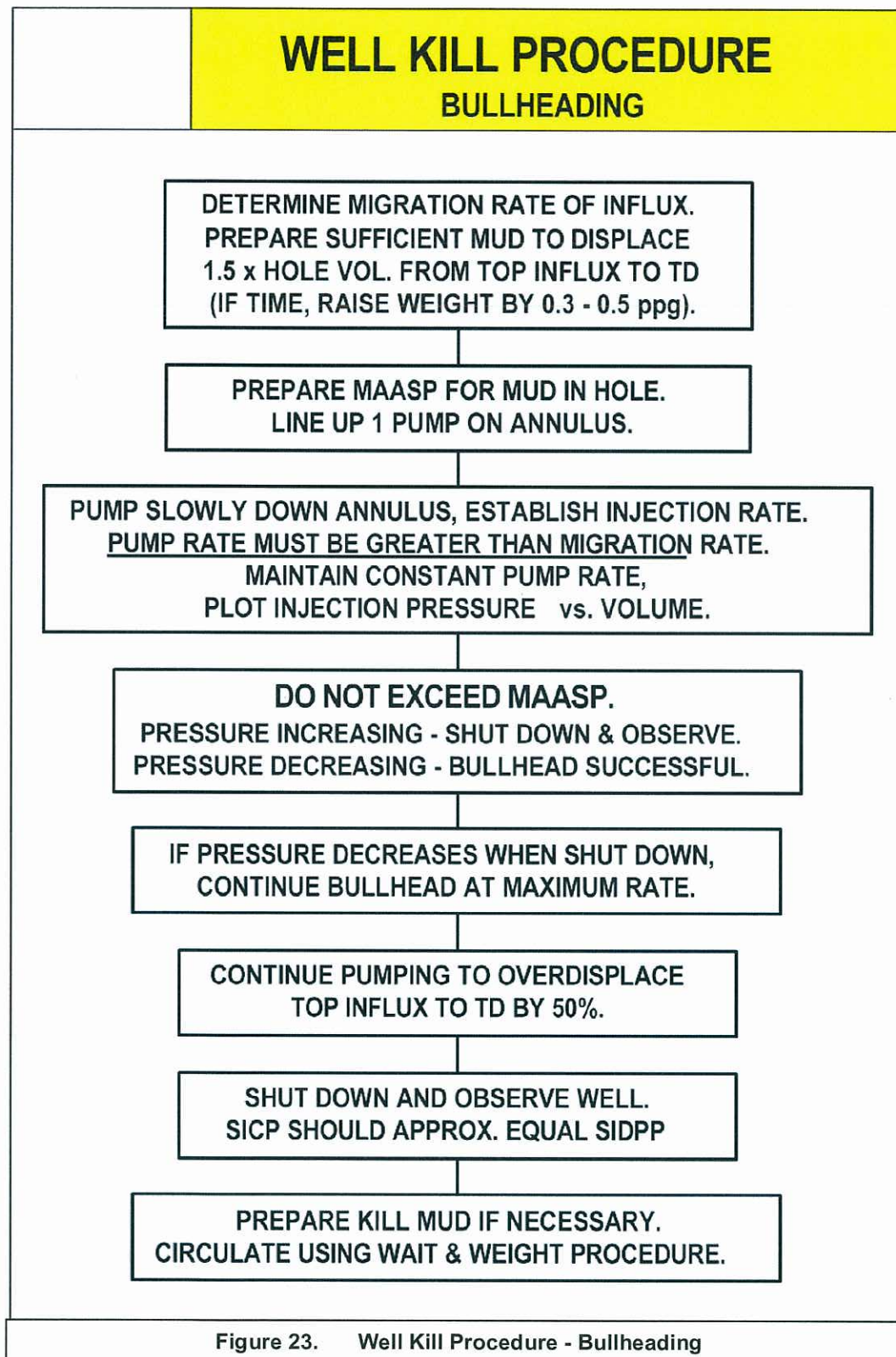


Figure 21. Well Kill Procedure – Volumetric Control Method (Casing Pressure)







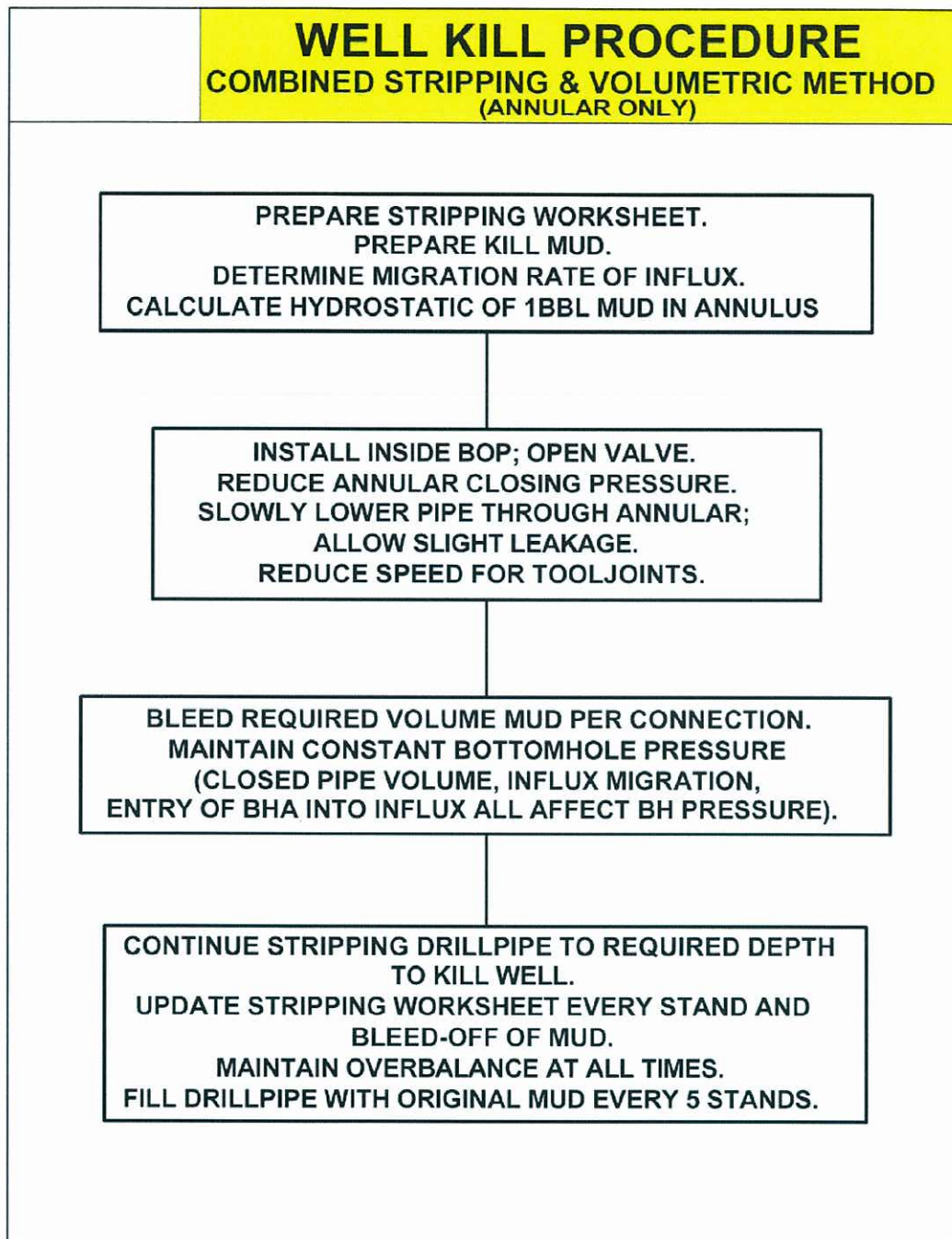


Figure 24. Well Kill Procedure – Combined Stripping & Volumetric Method (Annular only)